

HYENA (HYdro ENergy simulAtor)

Some Issues in a Simulation Model of a Hydro Thermal Power System.

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1. Introduction

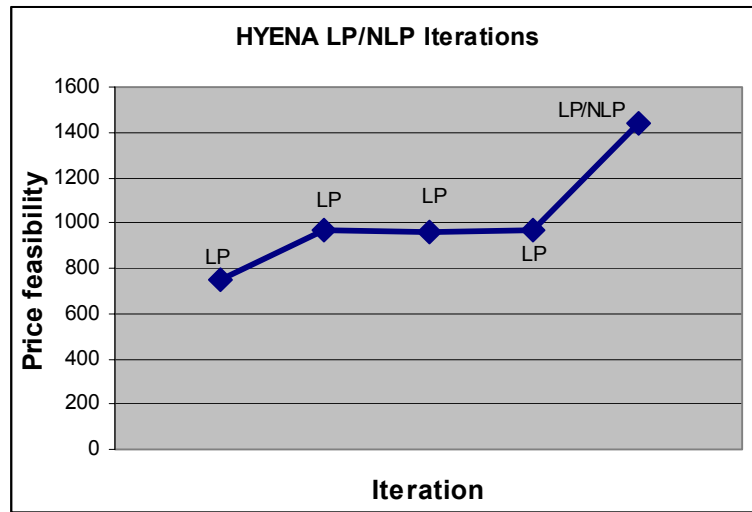
This report is a continuation of the report: "Simulation Model of Transmission Constrained Hydrothermal Power System" Skuli Johannsson, Annad veldi ehf, Reykjavik, Iceland and Elias B Eliasson, The National Power Company, Iceland, 01-August-2003. Revised 09-Dec-2003. The report can be found at <http://www.veldi.is/>

HYENA is based on a mathematical iteration process as follows:

- Read and prepare model data for Power system, Water series, Load demand etc for all operational years and water years.
- Start Iteration
 - Strategic part. Simplified description of System. Redefine load in water areas with information from last iteration as:
 - Demand
 - + Losses
 - - Transmission into Water Area
 - + Transmission from Water Area
 - + Selling activity on the Spot Market
 - - Buying activity on the Spot Market.
 - Calculation of water values for water areas taking into account local reserve power in water area.
 - Tactical part. Simulation of the Power System base on calculated water values for water areas, detailed description of the Production System, Transmission System and Load Demand in Substations.
 - Analyse results. If convergence then leave
- Repeat
- Print out Results
- End

Figure 1

The convergence of the iteration process is very efficient so usually three iterations give satisfactory result. The chart shows typical five iterations, first four using LP and the last using LP/NLP. NLP gives better result in this case.



The iteration process used in HYENA does not calculate exact

optimum solution which would take exponential time and computer resources. Instead the process finds an approximate solution trading optimality for efficiency. Such solutions, often loosely called *heuristic methods* or *heuristics*, seek to obtain good near-optimal solutions at relatively low computational costs sacrificing guarantee of optimality. The mathematical method used in HYENA, that iteratively improves the solution towards optimality, is in the literature referred to as *metaheuristic*. Example of this kind of methodology is the emerging technology of *Ant Colony Optimization* and *Genetic Algorithms*. From Mathematical Programming Glossary: "This is a general framework for heuristics in solving hard problems. The idea of 'meta' is that of level."

The biggest disadvantage of this approach is in sensitivity analysis but by tuning the HYENA model properly it has proven not to be a major problem. All kinds of sensitivity analysis can be performed with satisfactory and stable results.

As an advantage with HYENA one may argue that simulations are considered closer to reality than optimization with perfect foresight.

2. Hyena model Options

Following are the most important options available in HYENA and they can be mixed in any combination.

Optimization technique

- ✓ Linear Programming LP
- ✓ Mixed Integer Linear Programming NLP
- ✓ Nonlinear Programming
- ✓ Mixed Integer Nonlinear Programming

Constraints

- ✓ Without Transmission Lines
- ✓ Without Transmission/FlowGates Constraints
- ✓ With Transmission Constraints in Lines
- ✓ With Transfer constraints in FlowGates

Losses in transmission lines

- Nonlinear or Linear Losses

Time Unit

Week or Day

If NLP is used say for 5 iterations then in the first four iterations LP is used and in the last iteration the model first calculates an approximate solution before starting th NLP calculation. LP is 5-15 times faster than NLP depending on size of the model. Using the model for say 1 operational year, 51 water years, weekly time units 3 iterations, Linear Programming, and 30-40 hydro units takes ca 1 minute.

The chart shows typical results from HYENA for a small reservoir in a spotmarket environment. The figure shows swarm of reservoir curves of 50 water years with day as a time unit and using NLP. The thick water value curves give indication on when to buy or sell on the spot market. Between the curves there is neither buying nor selling, the system is in a waiting state.

Figure 2

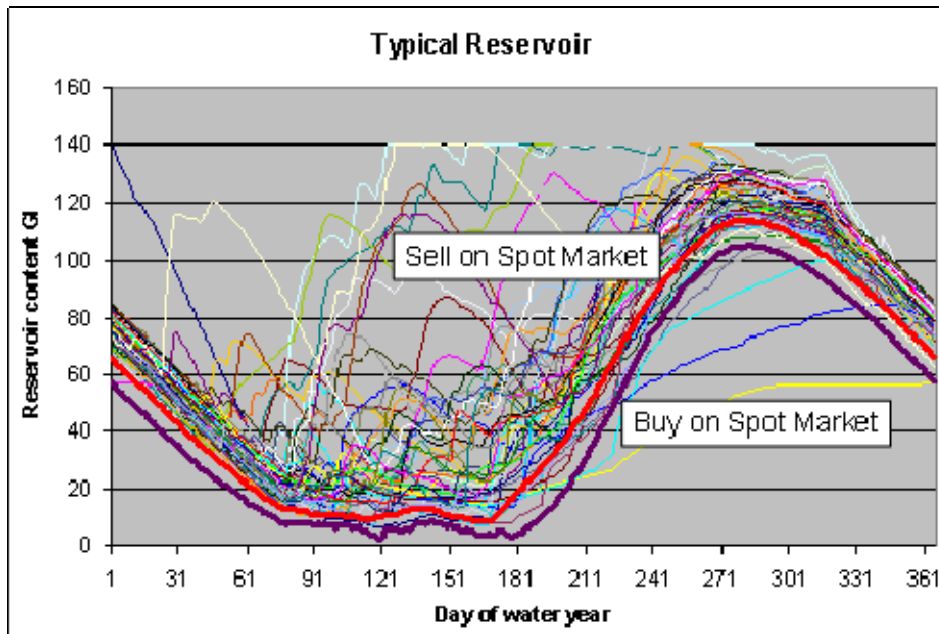


Figure 3 on the other hand shows a swarm of reservoir curves for a large reservoir in a non-spotmarket environment, 51 water years and 5 operational years with a time unit of 1 day and using NLP. The reservoir is assumed starting operation in 01.09.2006.

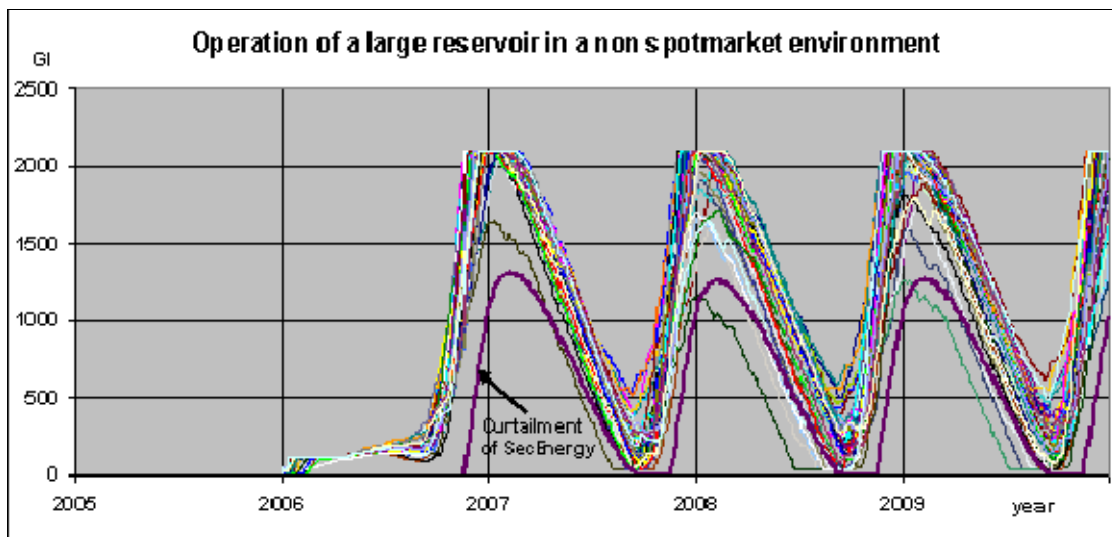


Figure 3

Detailed information as in figure 3 gives important guidelines on optimal timing, filling and subsequent operation of reservoirs in hydro power systems.

3. Operational years and water years

There are two setups in HYENA, the static setup and the dynamic setup

In the Static setup we have 1 operational year i.e. 2010 and say 51 water years say 1950-2000. We simulate over the 51 water year with the same demand (2010) every year. We start with specific reservoir content in the beginning of the first water year and the reservoir content in the end of one water year is the reservoir content in the beginning of next water year.

In the Dynamic setup we have >1 operational years i.e. 2004-2014. The Power System is simulated by the following schema:

Table 1
Dynamic setup of Operational years and Water years

No	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014
1	1950	1951	1952	1953	1954	1955	1956	1957	1958	1959	1960
2	1951	1952	1953	1954	1955	1956	1957	1958	1959	1960	1961
3	1952	1953	1954	1955	1956	1957	1958	1959	1960	1961	1962
4	1953	1954	1955	1956	1957	1958	1959	1960	1961	1962	1963
.
.
48	1997	1998	1999	2000	1950	1951	1952	1953	1954	1955	1956
49	1998	1999	2000	1950	1951	1952	1953	1954	1955	1956	1957
50	1999	2000	1950	1951	1952	1953	1954	1955	1956	1957	1958
51	2000	1950	1951	1952	1953	1954	1955	1956	1957	1958	1959

We start with specific reservoir content in the beginning of the first operational year 2004 and start with water year 1950. The reservoir content in the end of the year is the reservoir content in the beginning of operational year 2005 and water year 1951. We move like that horizontally until we come to the end of the row. Next we begin in second row with operational year 2004 and start with water year 1951 and continue horizontally throughout the rest of the schema. Water years are cycled so after the last water year 2000 comes again the first water year 1950.

In the Static setup is equivalent to moving down one column starting with the first water year 1950.

4. Strategic part

Water values are calculated in the strategic part.

First the Power System is subdivided into water areas. In each water area all hydro and geothermal stations are modelled together as a single power station with a single upstream reservoir. Substation with reserve stations and electricity market are placed within water areas. See figure 4.

Water values are expressed as a function of reservoir content in the water area and time.

$$\alpha(v_{wa}, t)$$

Calculation of water values is explained in figure 5. The vertical axis is divided into intervals and V_t is the reservoir content in one point. The single reservoir system is simulated one interval forward to time $t+1$ by the following model:

$$Q_{t+1} = Q_t + \alpha \cdot R_t + (w - \min(w, U_t))$$

Q_t is reservoir content in GWh, R_t is regulated inflow in GWh/week and U_t is unregulated inflow in GWh/week. α is aversion factor when drawdown of reservoir results in lower head at power stations. This constant is an input parameter and can be determined by experiment. It is usually on the interval 0,6 – 1,0. No variable head means $\alpha = 1,0$.

Figure 4. One Reservoir model of Water area in a Power System

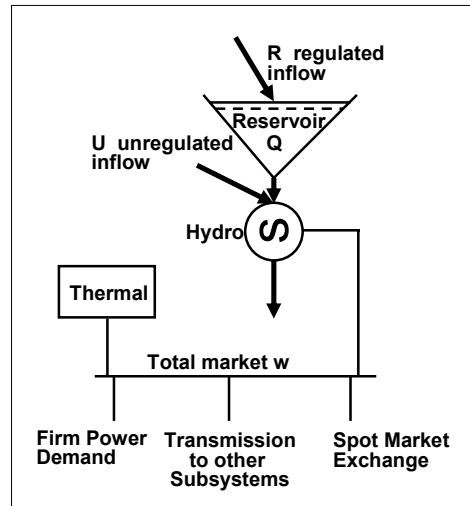
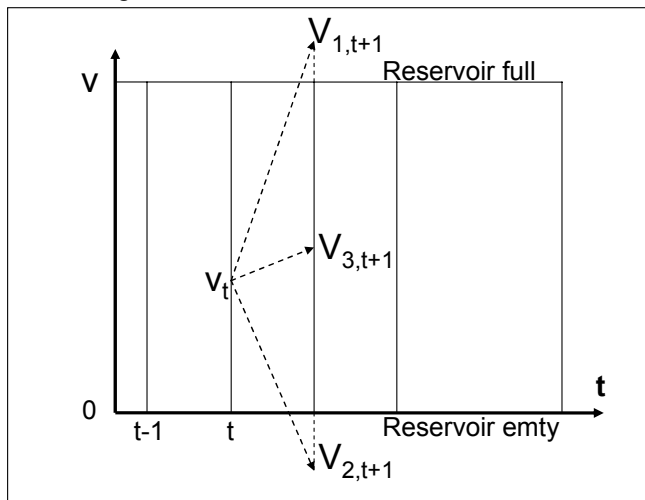


Figure 5. Calculation of Water Values

In calculating water values at V_t we simulate the system for all instances of river flow say 51 and we can have three possible outcomes according to fig 4:

1. Reservoir full $Q_{1,t+1} > Q_{max}$ then water value is = 0.
2. Reservoir empty $Q_{1,t+1} < 0$ then water value is equal to the variable cost of the last reserve unit (or curtailment price or spot market price etc) used to lift the reservoir level over 0.
3. Reservoir between empty and full then water value is the same as the water value at $V_{3,t+1}$ calculated by interpolation.



New water value at V_t is calculated by taking the average over all water years.

The whole procedure goes backward in time week by week or day by day and upwards from $Q = 0$ to $Q = Q_{max}$ in increments of say 2%. Usually 3 rounds in the water value schema results in a satisfactory convergence.

5. Tactical part

The Multiobjective function for every stage t of the planning period T is:

$$\min \left(\begin{array}{l} \sum_{j \in H_{Res}} \varphi \cdot \frac{\partial \rho}{\partial v_j} \cdot \alpha_{s,t+1} \cdot u_{j,t}^2 \\ + \sum_{j \in H_{ROR}} 0 \cdot u_{j,t} \\ + \sum_{j \in H_{All}} \xi \cdot \rho_k \cdot s_{j,t} \\ + \sum_{j \in Termal} c_j \cdot g_{j,t} \\ - \sum_{j \in Sell} c_j \cdot S_{j,t} \\ + \sum_{j \in Buy} c_j \cdot B_{j,t} \\ + \sum_{j \in Short} c_j \cdot g_{j,t}^2 \\ + \sum_{j \in Trans} \lambda \cdot L_{j,t}^+ + \lambda \cdot L_{j,t}^- \\ - \beta \cdot \sum_k \int_0^{v_{k,t+1}} \rho_k(x) \cdot \alpha_{s,t+1}(x) \cdot dx \\ + \sum_k \psi_a \cdot S_a \end{array} \right) \begin{array}{l} \text{Turbined water (Plants with Reservoirs)} \\ \text{Turbined water (Run-of-the-River)} \\ \text{Spilled water} \\ \text{Thermal} \\ \text{Selling on the Spot Market} \\ \text{Buying on the Spot Market} \\ \text{Power Shortage} \\ \text{Transmission} \\ \text{Reservoirs} \\ \text{Spinning Reserve requirements} \end{array}$$

Continuity equation for electricity in substations:

$$\begin{array}{l} \sum_{i \in s} \rho_i(v_t) \cdot u_{i,t} \\ + \sum_{j \in T,S} g_{j,t} \\ - \sum_{j \in s} B_{j,t} \\ + \sum_{j \in S} S_{j,t} \\ - \sum_{n \in s} L_n^+ \\ + \sum_{n \in s} L_n^- - a \cdot L_n^{-,2} - b \cdot L_n^- - c \\ = w_{s,t} \end{array} \begin{array}{l} \text{Hydro Production} \\ \text{Thermal Production and Shortage} \\ \text{Buying on the Spot Market} \\ \text{Selling on the Spot Market} \\ \text{Transmission from substation} \\ \text{Transmission to substation} \\ \text{Load in substation} \end{array}$$

Water balance for every hydro power station; continuity equation for water:

$$v_{i,t+1} = v_{i,t} - u_{i,t} - s_{i,t} + r_{i,t} + \sum_{m \in U_i} [u_{m,t} + s_{m,t}] \quad (3)$$

Limits on reservoir storage: $v_i^{\min} \leq v_{i,t} \leq v_i^{\max}$ (4)
(Rule Curves, fish conservation, environmental constraints etc)

Limits on turbined water: $u_i^{\min} \leq u_{i,t} \leq u_i^{\max}$ (5)
(Maintenance, environmental constraints etc)

Limits on spilled water: $s_i^{\min} \leq s_{i,t} \leq s_i^{\max}$ (6)
(Environmental constraints etc)

Limits on thermal generation: $0 \leq g_{j,t} \leq g_j^{\max}$ (7)
(Limits on curtailment)

Curtailment of secondary energy:

- Max 50% every year
- Max 40% every 4 consecutive years
- Max 20% every 20 consecutive years

Fairness between I customers in curtailment of secondary energy.

$$\sum_{j \in \text{Curt}} \frac{g_{j,t}}{g_j^{\max}} = \text{Either } I \text{ or } 0 \text{ (integer variable)}$$

Transmission line capacity: $L_n^+ \leq L_n^{\max} \quad L_n^- \leq L_n^{\max}$ (8)

Limits on transmission capacity in Flow Gates (FG):

$$\begin{aligned} \sum_{n \in FG} f_n^+ \cdot L_n^+ + \sum_{n \in FG} f_n^- \cdot L_n^- &\leq L_a^* \\ \sum_{n \in FG} (1 - f_n^+) \cdot L_n^+ + \sum_{n \in FG} (1 - f_n^-) \cdot L_n^- &\leq L_a^* \end{aligned} \quad (9)$$

Spinning reserve requirement in hydro and geothermal plants for each area:

$$\sum_{i \in a} \rho_i(v_t) \cdot u_{i,t} - S_a \leq (1 - \sigma_a) \cdot \sum_{i \in a} \rho_i(v_t) \cdot u_i^{\max} \quad (10)$$

Note: The definitions above refer to the HYENA Option: *Mixed Integer Nonlinear Programming, with Transfer constraints in transmission lines and flowgates and Nonlinear losses*. All other options in chapter 2 are subsets of this general option.

6. Definitions

t :	time index
T :	planning period
a :	area index
s :	subsystem index
k :	reservoir index
j :	thermal plant index
i :	hydro plant index
m :	index for upstream hydro plants
n :	transmission line index
$V_{i,t}$	Stored volume at plant i at the beginning of stage t
$V_{i,t+1}$	Stored volume at plant i at the end of stage t
$r_{i,t}$	Lateral river flow arriving at power station i in stage t
$u_{i,t}$	Turbined outflow at power station i in stage t
$u_{i,t}$	Spilled outflow at power station i in stage t
U_i	Set of hydro plants immediately upstream of plant i
$g_{j,t}$	Generation of thermal plant j in stage t
c_j	Generation cost of thermal, shortage and prices on spot market
B_j	Buying on Spot Market (Defined for peak and off-peak load)
S_j	Selling on Spot Market
$\sum_j c_j \cdot g_{j,t}$	The immediate thermal operating cost in stage t
φ	Factor in penalty function for turbined water (0,4-1,0)
ξ	Penalty for spilling water
λ	Damping factor for transmission (i.e. 0,00003)
$\sum_k \rho_k(v_{t+1}) \cdot \alpha_{k,t+1} \cdot v_{k,t+1}$	The future cost represented by:
$\rho_k(v_{t+1})$	The production coefficient of reservoir k [kWh/kl]
$\alpha_{s,t+1}$	The water value for subsystem k [kr/kWh]
$v_{k,t+1}$	Reservoir volume at the end of stage t [kl]
β :	Discount factor
L_n^+	Transmission in positive direction between subsystems
L_n^-	Transmission in negative direction between subsystems
τ_n	Transmission losses
L_{FG}^*	Limit on transmission in Flow Gates.
f_n^+	=1 if direction of transmission line is the same as direction of Flow Gate, else=0.
f_n^-	=1 if direction of transmission line is the opposite to direction of Flow Gate, else=0.
ψ_a	Penalty factor for spinning reserve requirement in area
S_a	Lack of spinning reserve
σ_a	Spinning reserve requirements, i.e. $\sigma_{week}=0,10$ and $\sigma_{day}=0,075$
$W_{s,t}$	Energy market in a subsystem
$W_{a,t}$	Energy market linked to a spinning reserve group.

7. Supply and Demand

In deregulated power systems market equilibrium is established where the supply (marginal cost) and demand curves meet, which defines competitive quantity on the market and market price as described in figure 6.

The *demand curve* represents that in nearly all markets quantity demanded rises as price falls; buyers wish to buy more at lower price and less at higher price. If the demand curve is vertical price changes will not affect the buying behavior of the consumer.

The *supply curve* represents that at lower prices, suppliers are less willing or capable of producing. The slope of the curve can be zero if suppliers are able because of their costs to supply more output at the same cost as with hydro power in Iceland in off critical periods.

Consumer surplus is the difference between the market price and what customers would have been willing to pay and *producer surplus* is the difference between the market price and at what price producers would have been willing to produce. Social surplus is the sum of consumer and producer surplus.

Figures 7-9 show examples of supply/demand curves and represents actual data calculated in the HYENA Simulation Model.

Figure 7 shows typical supply and demand curve for the South-West area of Iceland which has predominantly hydro power. Curtailment option is both included in the supply and demand curve.

Figure 6 Market mechanism

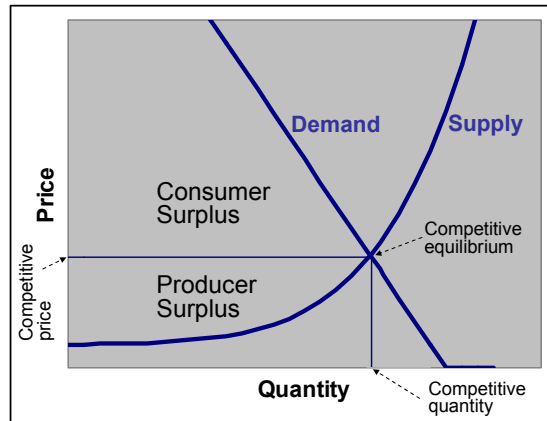


Figure 7

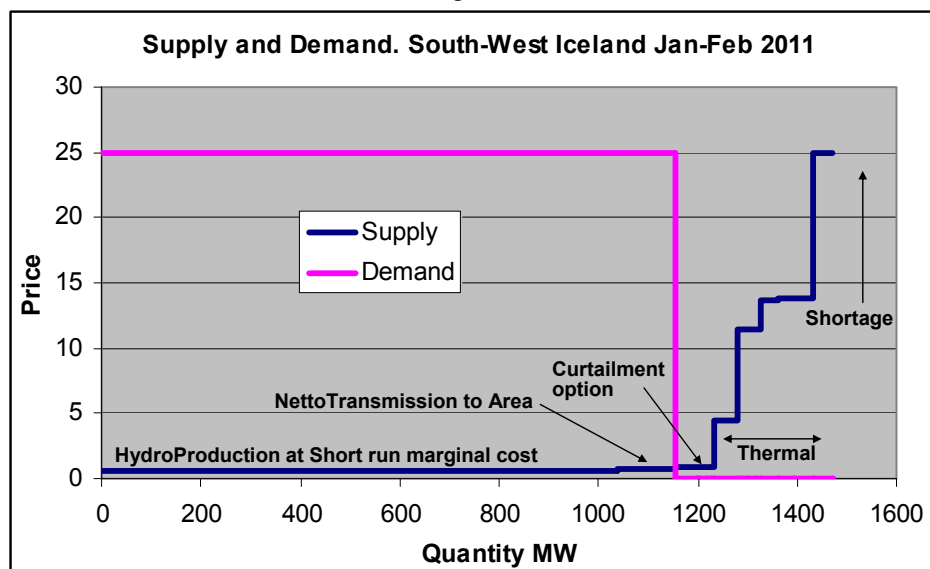


Figure 8 shows supply and demand curves for a small power system connected to an active spot market. In this situation the customer is buying from the market and Hydro Power has been diminished to a minimum to collect water in reservoirs.

Figure 8

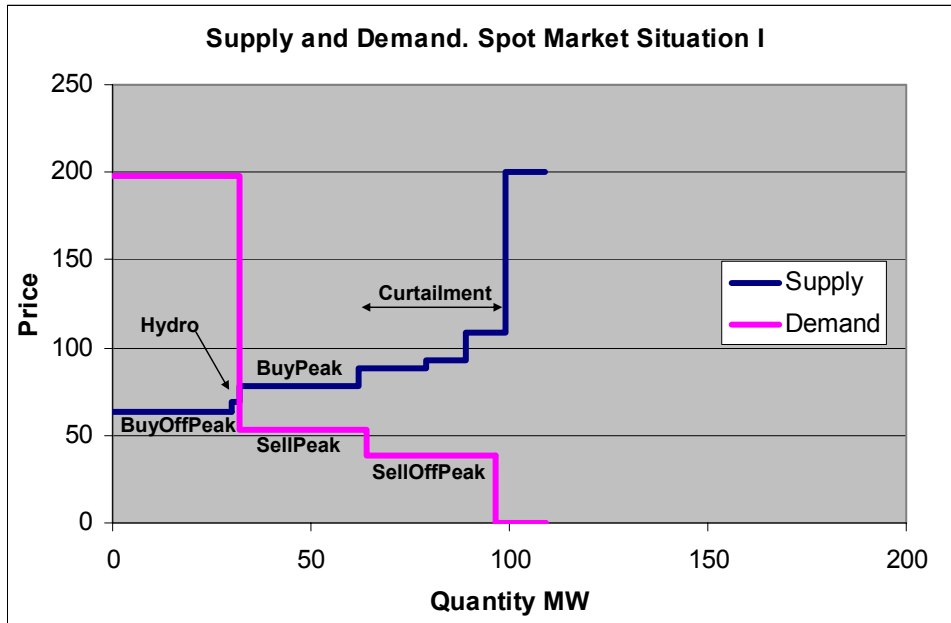


Figure 9 shows for the same system a situation with much more Hydro Power Production a part of which is sold on the market (Sell Peak).

Figure 9

